



ACI/PCI CODE-319-25
Structural Precast Concrete—Code Requirements and Commentary
Reported by Joint ACI/PCI Committee 319
Errata may already be included in the print version you own

ERRATA as of May 19, 2026

Section 22.65.6.2.4, pg. 198, Updated section number as shown:

22.5.6.2.4 In composite members, the principal tensile stress shall be calculated at the location specified in ~~22.5.6.3.3~~ 22.5.6.2.3 for the composite section, considering superposition of stresses calculated cross sections that resist the corresponding loads.

Section 22.55.6.2.1(c), pg. 196, Update equation as shown:

$$\cancel{V_{ci} = \lambda \sqrt{f'_c} b_w d} \quad \underline{V_{ci} = 2 \lambda \sqrt{f'_c} b_w d}$$

ERRATA as of May 11, 2026

Section 18.13.5.10.5, pg. 175, replace Eq. (18.13.5.10.5(d)) as follows:

$$\cancel{A_{sh} = 0.3 s b_c \left(\frac{f'_c}{f_{yt}} \right) \left(\frac{A_g}{A_{ch}} - 1.0 \right) \left(0.5 + \frac{1.4 P_u}{f'_c A_g} \right)} \quad (18.13.5.10.5d)$$

$$\underline{A_{sh} = 0.12 s b_c \left(\frac{f'_c}{f_{yt}} \right) \left(0.5 + \frac{1.4 P_u}{f'_c A_g} \right)} \quad (18.13.5.10.5d)$$

Change lettering in the following instances:

R26.4.2.1	242	(a)(10)(iii) ... If the quantity of Type A, B, or C mineral filler derived from carbonate aggregate proposed for use is such that the total calcium carbonate content from cement and mineral filler is equal to or less than 15 percent by mass of the cementitious materials, then sulfate resistance can be evaluated by ASTM C1012 to comply with the expansion criteria in Table 26.4.2.2(eb).
	243	(a)(11)(ii) Because of its high alkali content, use of ASTM C1866 Type GS ground-glass pozzolan in concrete made with potentially alkali-silica reactive aggregates should be avoided in W1 and W2 exposures unless data showing satisfactory concrete prism expansion in accordance with ASTM C1293 are available following the guidance provided in ASTM C1778. Refer to R26.4.2.2(eb)

26.4.2.2	244	(b) For concrete mixtures to be used in members identified in construction documents to be exposed to sulfate, alternative combinations of cementitious materials to those specified in 26.4.2.1(a)(910) are permitted if tests for sulfate resistance satisfy the criteria in Table 26.4.2.2(b).
R26.4.2.2	244	(b) ... The expansion criteria in Table 26.4.2.2(eb) for testing in accordance with ASTM C1012 are the same as those in ASTM C595 and C1157 for moderate sulfate resistance (Optional Designation MS) in Exposure Class S1 and for high sulfate resistance (Optional Designation HS) in Exposure Class S2 and Exposure Class S3 Option 2.
	245	(d)(1) ... If calculated total chloride ion content exceeds the limits in Table 19.3.2.1, the concrete materials can be adjusted until compliance is achieved, or water-soluble chloride ion content can be determined using 26.4.2.2(ed)(2).

ERRATA as of February 23, 2026

Section 2.2, pg. 16, move notation f_{pd} from the Commentary column to the Code column.

the flange, due to both prestress and moments resisted by precast member acting alone

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f_{pd} = stress in partially developed pretensioning strand when considering end region strength using moment equilibrium, psi

f_{pe} = compressive stress in concrete due only to effective prestress forces, after allowance for all prestress losses, at extreme fiber of section

Section 18.5.4, pg. 162, Change the title of 18.5.4 to the following:

18.5.4 Joints in intermediate precast structural walls

Section 18.12.11.4(c), pg. 172, change 22.9.4.6 to 22.9.4.5.

(c) The area of reinforcement required to resist a net factored tension across a joint in the precast concrete diaphragm shall be added to the area of reinforcement required for shear friction crossing the joint, in accordance with ~~22.9.4.6~~ 22.9.4.5.

Section 24.5.3.2 and R24.5.3.2, pg. 228, change f_c' to f_{ci}'

Table 24.5.3.2—Concrete tensile stress limits immediately after transfer of prestress, without additional bonded reinforcement in tension zone

Location	Concrete tensile stress limits
Ends of simply supported members	$6\sqrt{f_c'}$ $6\sqrt{f_{ci}'}$
All other locations	$3\sqrt{f_c'}$ $3\sqrt{f_{ci}'}$

$$3\sqrt{f'_{ci}}$$

$$6\sqrt{f'_{ci}}$$

R24.5.3.2 The tensile stress limits of ~~$3\sqrt{f'_c}$~~ and ~~$6\sqrt{f'_c}$~~ refer to tensile stresses at transfer of prestress at locations other than the precompressed tension zone. Where tensile stresses exceed the permissible values, the total force in the tensile stress zone may be calculated and reinforcement proportioned on the basis of this force at a stress of $0.6f_y$, but not more than 30,000 psi. The effects of creep and shrinkage begin to reduce the tensile stress almost immediately; however, some tension remains in these locations after allowance is made for all prestress losses.

ERRATA as of August 6, 2025

Section R22.7.5, pg. 204:

There is missing text under one of the square root symbols. Replace $\sqrt{\quad}$ with $\sqrt{f'_c}$.